Harmonics Reduction Using Adaptive Notch Filter Based Active Power Filter

Abhilash Purohit *, Smita Sahoo, Debaswarup Rath
Department of Electrical Engineering
Gandhi Institute for Education and Technology, Baniatangi, Bhubaneswar

Mr. Aruna Rout, Department of Electrical EngineeringCapital
Engineering College, Bhubaneswar

ABSTRACT

In this work the application of adaptive notch filter (ANF) is implemented as reference signal technique for active power filter (APF) for harmonics analysis in three phase system. Here two different techniques like direct and indirect control techniques are used. The benefit of utilizing the ANF technique is based on its easy design which provides the ANF advantages to be utilize in microcontroller. The operation of the ANF is analysed though MATLAB simulation in ICC and DCC configurations. The ANF is proficient to work proficiently for both ICC and DCC modes, but in term of efficiency, the ICC mode is noticeably presenting a better harmonics mitigation result. Base on the result also it shown that the ANF is capable of mitigate the harmonics below the standard required by the IEEE 519-92. The use of ANF is suitable to be applied due to its simple design and filtering technique.

1. INTRODUCTION

The needs of power quality compensation in electrical power system is becoming more and more crucial nowadays as the increase of the development in power electronics equipment. The trends of power electronic applications are soaring whether within industrial applications or throughout domestic applications. This abundancy leads to the pollution of the electrical power system, which is mostly harmonics [1]. Mitigation or suppressing the harmonics has been suggested within these recent yearsas the research works in active power filter (APF) have been progressing. This paper specifies on the strategyof extracting the harmonics in order to support the control of the APF.

In developing an APF, one of most important components is the harmonics extraction algorithm. This algorithm functions as the core component in supplying the reference signal to the APF for producing compensative power to the electrical power system. In developing the extraction algorithm, many methods have been studied and applied whether in time or frequency based domains. In frequency based domain, the techniques used are ranging from fast Fourier and discrete Fourier series [2–5], Kalman filtering [6-8] and wavelet transformation [9]. However, working in the frequency domain is a little tedious as it involves transformation of information into frequency domain. The commonly used extraction techniques for the APF is within the time domain as it will involve the algorithm to work in real time condition. The time domain is divided into classical methods such as PQ and PQR theory [10-13], synchronous reference frame theory [14-16], and capacitor voltage control techniques. Alternatively, the intelligent techniques have been considered such as neutral network [17], adaptive neural network and adaptive linear neuron [18-21]. Besides the three groups of techniques used widely, another emerging technique is the filtering technique such as adaptive notch filter (ANF), in which this technique has simple design and does not require training.

This paper proposes application of ANF based on the IIR filter as an extraction method of harmonics for indirect current control (ICC) and direct current control (DCC) of APF. By applying the ANF, the filter is capable of tracking the frequency and phase of the system without additional component such as phase lock loop (PLL). Another advantage of applying the ANF is its capability to filter out the fundamental component and selective components of harmonics of the electrical power system.

2. PRINCIPLE OF ADAPTIVE NOTCH FILTER

An ideal notch filter is a filter that allows a linear gain at every frequency except at a specified frequency where the gain is zero. Based on this condition, the notch filter is able to withdraw the solicit signal of sinusoidal components from electrical power system within the given frequency.

2.1. Adaptive notch filter design

Initially, ANF is designed based on the IIR filter but operating within the frequency domain. However, later on the ANF is transposed into the time domain in order to suite within the time based operation [22]. For better dynamic condition, the ANF is then modified in scalar condition with adaptation mechanism. The dynamic behavior of ANF can be proposed as the following set of differential equations [23, 24].

$$\ddot{x} + \theta^2 x = 2\varepsilon\theta e\,(t) \tag{1}$$

$$\dot{\theta} = -yx\theta e\,(t) \tag{2}$$

$$e(t) = u(t) - \dot{x} \tag{3}$$

From the set of equation, the system can be explained as following condition. The input signal of the system is given as u(t), θ represents the estimation frequency of the system while ε and γ represent two coefficients that play important role in determining the accuracy and the convergence speed of the system. The two coefficients are randomly set but both values need to compensate each other or otherwise the ANF will not function at its maximum filtering capacity [25]. In a functional single sinusoidal input u(t)=A_1 sin ($\omega_0 t + \phi_1$) , the used ANF has an explicit characteristic where it is having a unique periodic orbit located at . Based on the output of the ANF, the filter will produce the cos component of the filtered signal

$$O = \begin{pmatrix} \bar{x} \\ \dot{\bar{x}} \\ \bar{\theta} \end{pmatrix} = \begin{pmatrix} \dfrac{-A_1 \cos(\omega_0 t + \varphi_1)}{\omega_0} \\ A_1 \sin \omega_0 \,(\omega_0 t + \varphi_1) \\ \omega_0 \end{pmatrix}$$

noted by x but with negative magnitude and sin component is noted by $\dot{x}$ but the value of the sin needs to be scalar with in order to get right value of filtered input [26, 27]. The basic structure of the ANF for single-phase system is shown in Figure 1.
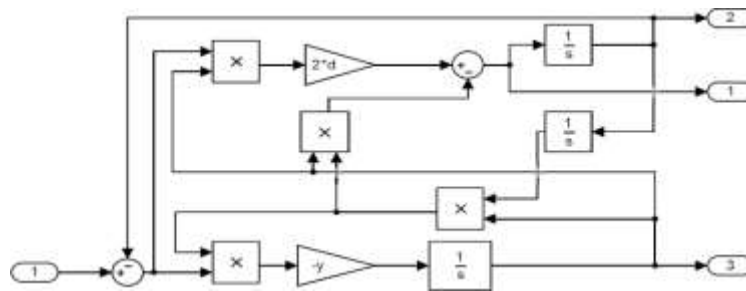

Figure 1. ANF structure for single-phase system

2.2. Three-phase ANF

As shown in the previous section, a singular set of ANF works only for a singular input signal. In order to design a functional three-phase ANF, the arrangement can be generalized to a sequence of three ANFs which will be working in parallel to extract the fundamental components of each of the input signals. Since the structure of the three-phase ANF is having the same frequency over time, the frequency estimator of the system can be shared between them, thus reducing the integration function of the three-phase system [28]. This approach therefore provides decrease in error over preceding method as the ANF is sharing the frequency estimator. Basically, the ANF for three-phase usage is defined by following equations.

$$\ddot{x}_n + \theta^2 x_n = 2\varepsilon\theta e_n(t) \tag{4}$$

$$\theta = -y\theta \sum x_n e_n(t) \tag{5}$$

$$e_n(t) = u_n(t) - \dot{x}_n \tag{6}$$

where n is the phase (a, b and c) and the update law on the frequency is summation of the error and the signal of all three phases.

The design of the three-phase ANF is shown in Figure 2. It is shown that the ANF structure is divided into two, in which the first structure is the generalized frequency extractor where it is composed from (5) and the second structure is the component extraction [29]. It can be seen that the ANF works by updating the error law in (6) of each individual phase of signal.
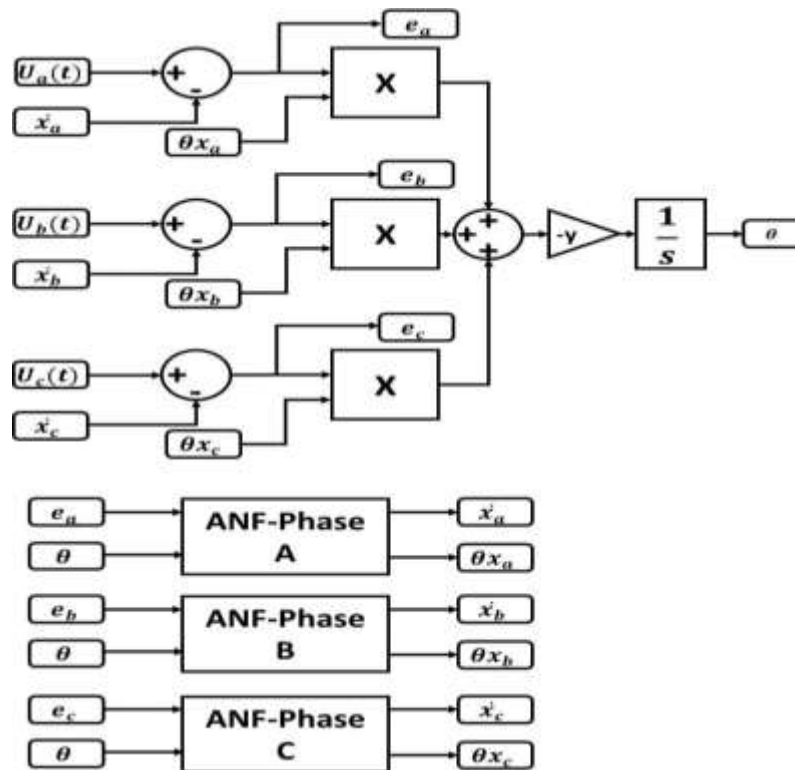

Figure 2. ANF structure for three-phase system

3. CURRENT CONTROL METHOD OF ANF

The proposed ANF is designed and simulated in a three-phase shunt APF. The configuration of three-phase shunt APF with ANF as the harmonics extraction is shown in Figure 3. The system is consisting of a three-phase power supply, shunt APF and nonlinear load. The source of harmonics is deviated from the nonlinear load where it consists of three-phase rectifier circuit and attached with an inductive load. For the shunt APF, control strategies are made of harmonics extraction algorithm, current control algorithm and switching algorithm. In this paper, the main extraction algorithm is the ANF where the highlighted item is on the implementation of ANF ICC and DCC modes. The switching algorithm is implemented with hysteresis switching control. As shown in Figure 3, the source current is summation of the load current and the harmonics current as in (7).

$$I_s = I_L + I_H \tag{7}$$

The reference current signal of the shunt APF can be taken from two mentioned current control methods. For the ICC, the ANF will produce the filtered fundamental input current signal and the signal then will be compared with the supply input current. The difference between both signals will be taken as the input for the shunt APF but with inverse magnitude. This condition is given as follow.

$$I_{comp} = I_{load} - I_{fund} \tag{8}$$

Meanwhile, for the DCC, the harmonics signal generated by the ANF is compared to the filter current that are produced by the shunt APF. The harmonics needed for this control is taken from the error value of the ANF as given in (6). The current control is given as (9). The signal given to the shunt APF is the additional value required for filter to reach compensation error between the harmonics signal of the ANF and filtering current.

$$I_{comp} = I_{H+ANF} - I_{H+SAPF} \tag{9}$$

4.   SIMULATION RESULT AND ANALYSIS

The capabilities of the proposed extraction algorithm is tested and validated by a simulation tool. The simulation is done using MATLAB Simulink with sim power system toolbox. Figures 3 and 4 show the simulation diagram of APF with the ANF for both DCC and ICC modes. The simulation parameters considered are shown in Table 1. In order to obtain the appropriate response of the system, the simulationis done within this order, initially the load is turned off and when the time reaches 0.1s, the load is truned on, and when the time reaches 0.3s, the APF is connected to the point of common coupling (PCC).
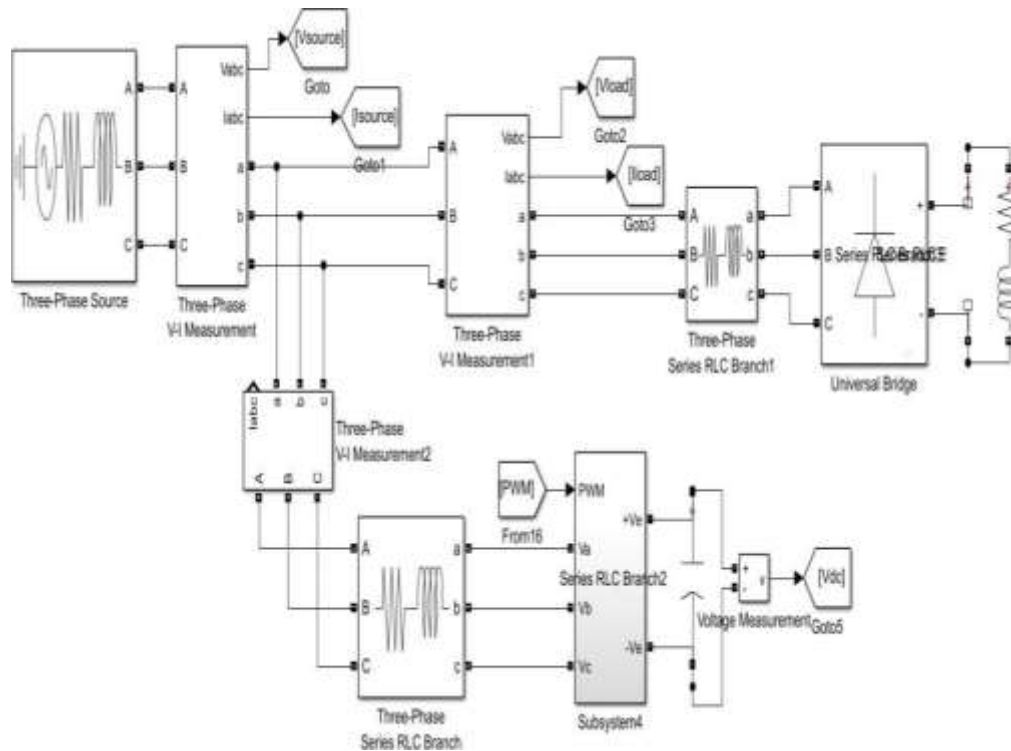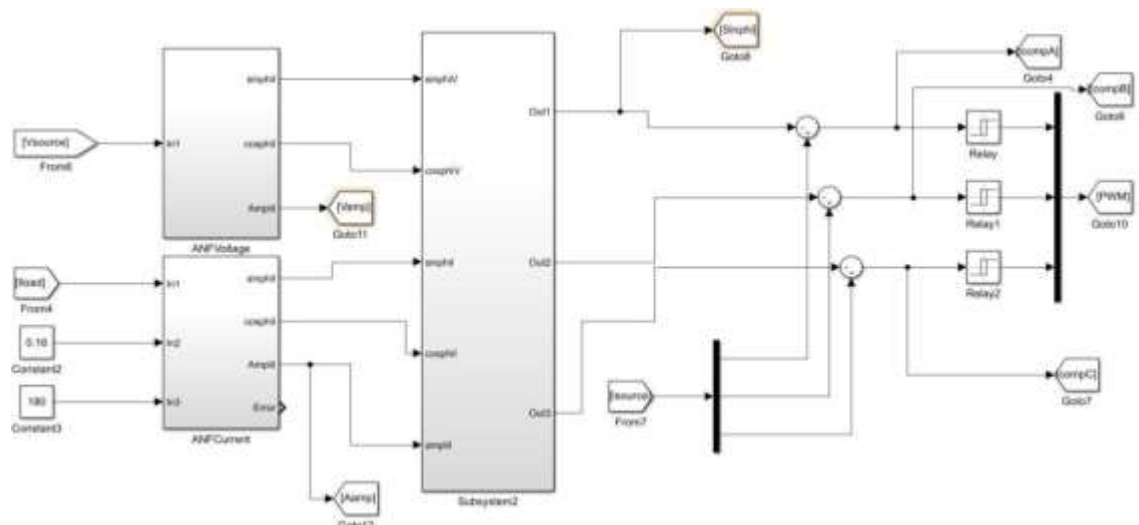

Figure 3. Shunt APF for three-phase system

Figure 4. ANF structure in MATLAB Simulink

Table 1. Simulation parameters

Parameter	Value
Source Voltage	415 V (RMS), 50 Hz
Source Impedance	1Ω, 1mH
Single Phase Nonlinear Load	60 Ω, 50 mH
DC Link Capacitance and Vref	3300 μF, 700V
Filtering Inductor	5 mH
ANF Gains	ε=0.16, y=180

4.1. Indirect current control

The first simulation is done in order to demonstrate performance of the ANF for ICC. Figure 5 (a) shows the source voltage and load voltage within all the simulation stages. As shown in the figure, the source and load voltage waveforms are maintained during all of stages without being affected by the turning of load and APF. Figure 5 (b) shows the source current and load current for the APF with ICC mode. From the figure, the system starts to operate the load at 0.1s, at this point the source and load currents are having non-ideal sinusoidal waveforms. However, when the APF is applied to the system at 0.2s, the harmonics are managed to be compensated where the current source managed to regain the sinusoidal waveform. The detailed waveforms of source voltage, source current and filter current at the PCC is shown in Figure 6. The figure clearly shows that the source is successfully mitigated by the APF and waveform of the compensation current at the filtering inductor.
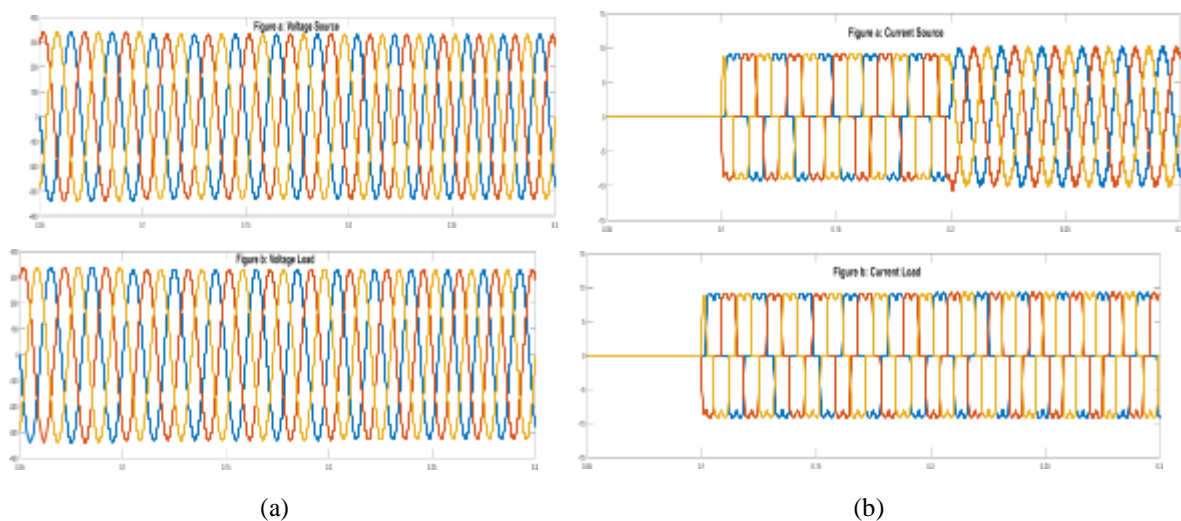

(a)

(b)

Figure 5. (a) Source voltage and load voltage for ICC, (b) Source current and load current for ICC
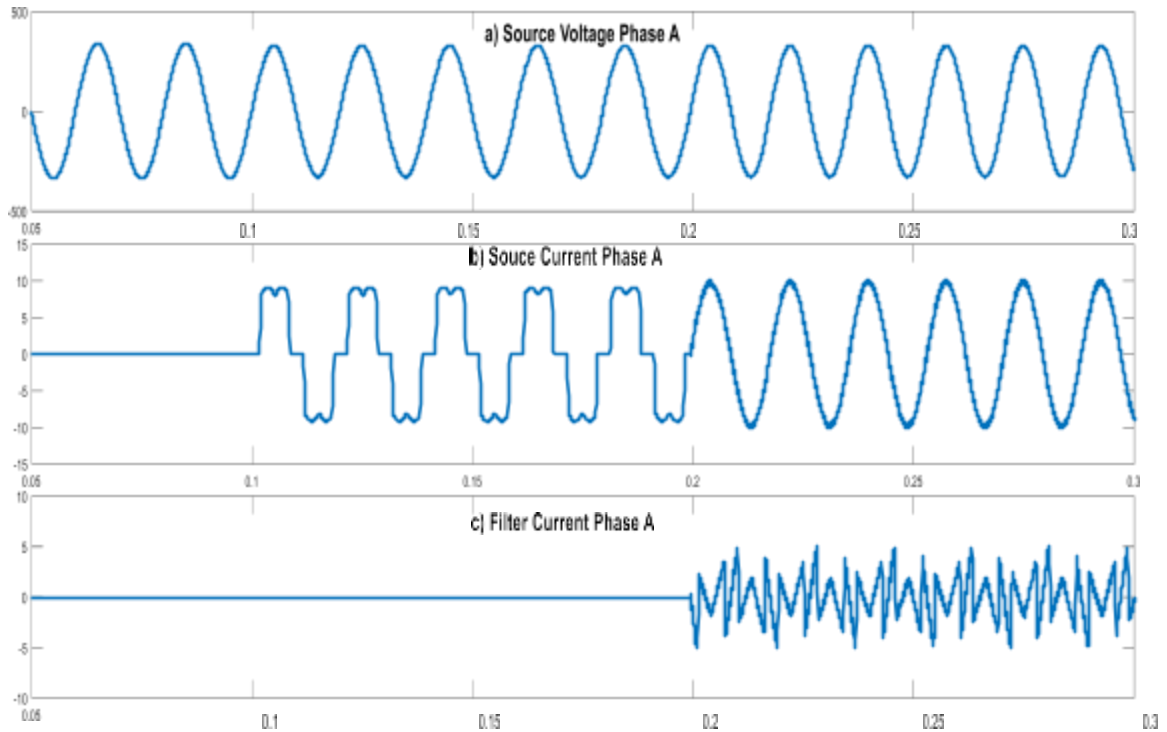
Figure 6. Phase A ICC waveform, (a) Source voltage, (b) Source current and (c) Filter current

4.2. Direct current control

The second simulation is done for the ANF using DCC method with the same system specification. As same as the predecessor method, the source and load voltages are maintained during the systemis introduced to load and APF as shown in Figure 7 (a). Comparable with ICC method, the DCC method also manages to mitigate the source current when it is applied to the system, and the undesirable sinusoidal waveform that affecting the source current contributed by the load is managed to regain the desire sinusoidal shape. This shows that the APF functions accordingly in reducing the harmonics within the system.As shown in Figure 7 (b), at point 0.2s, the source current from each phase changes the shape intoa sinusoidal waveform. In Figure 8, the detailed waveform of the DCC for phase A is shown. The figure show the source voltage, the source current and the filter current. When the APF is activated at point 0.2s and upon operation, it manages to mitigate the harmonics.

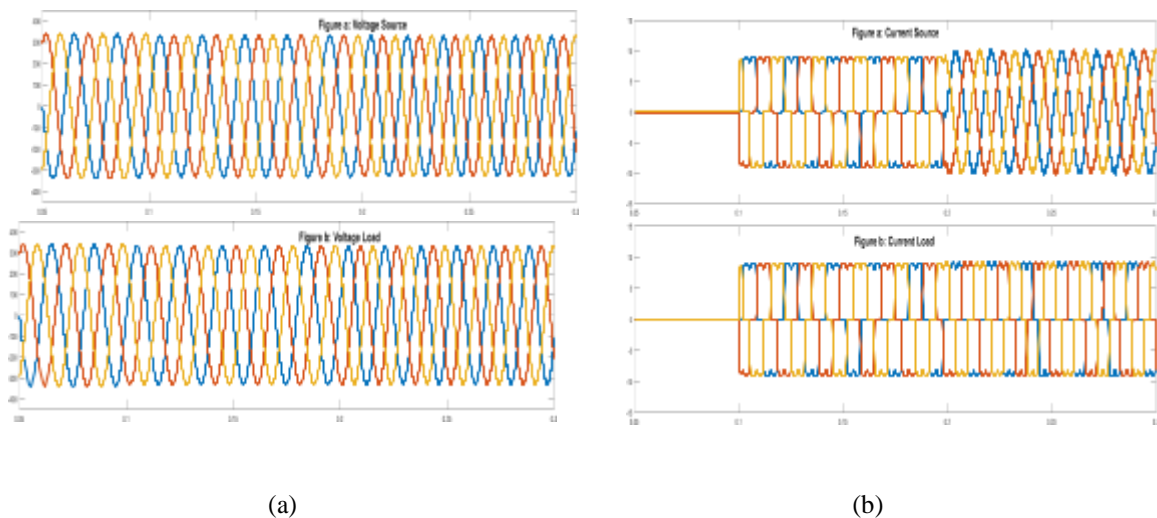(a)   (b)

Figure 7. (a) Source voltage and load voltage for DCC, (b) Source current and load current for DCC
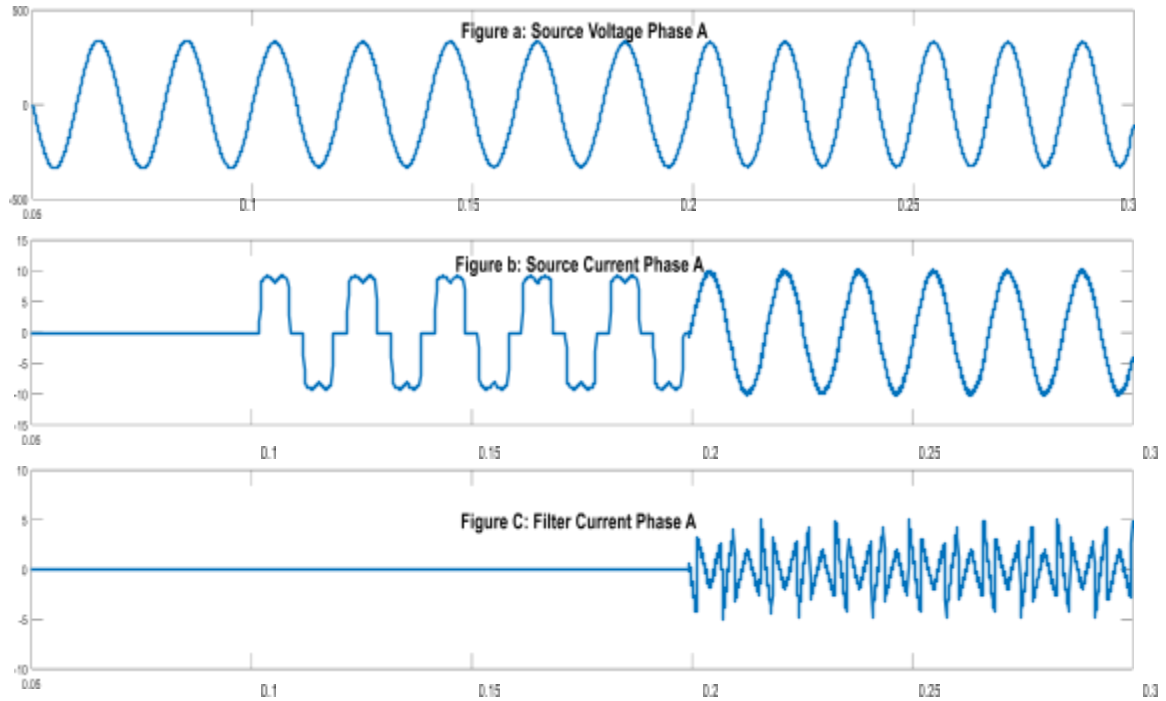
Figure 8. Phase A DCC waveform, (a) Source voltage, (b) Source current, and (c) Filter current

4.3. Total harmonic compensation

Both ICC and DCC modes perform as expected in controlling the harmonics of the source current at PCC. Based on the initial condition of the system without the APF, the harmonics measured is around 27.97%, and when APF is applied, the harmonics are reduced to 2.01% and 2.43% for ICC and DCC respectively, as shown in Figure 9. The recorded total harmonic distortion (THDs) for all phases before and after mitigation are shown in Table 2. Based on this result, it is shown that APF with ICC is having better performance in mitigating harmonics compared to DCC. However, both are still ensuring APF to operate within the limit IEEE standard, which is below 5%.

Table 2. THD's measured for ICC and DCC

PHASE	ICC		DCC	
	Without APF	With APF	Without APF	With APF
PHASE A	27.97 %	2.01 %	27.97 %	2.43 %
PHASE B	27.97 %	1.99 %	27.97 %	2.44 %
PHASE C	27.97 %	2.01 %	27.97 %	2.46 %

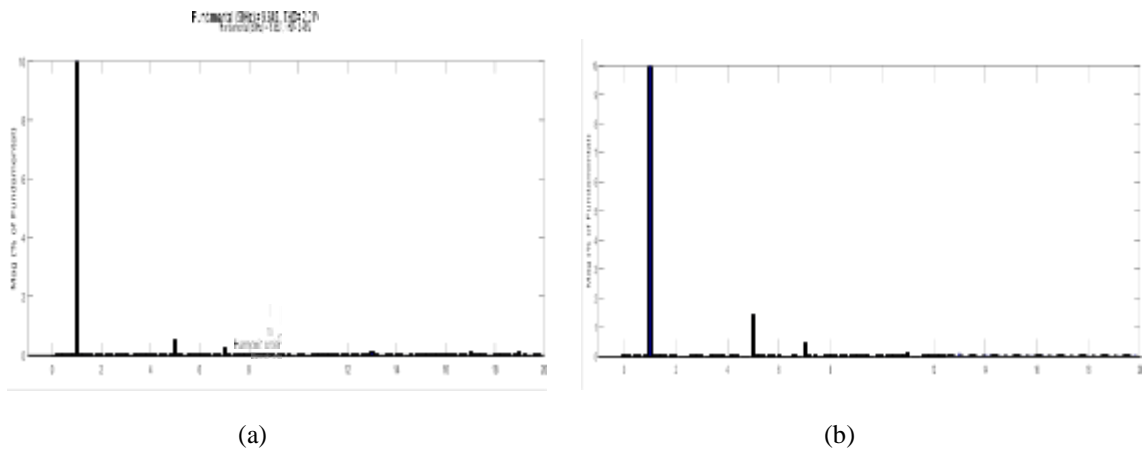(a)   (b)

Figure 9. THD of phase A for, (a) ICC method, (b) DCC method

5. CONCLUSION

In conclusion, ANF has been used in the shunt APF as harmonics extraction method for two current control methods. The work as demonstrated in the simulation is capable of extracting both fundamental and harmonics signals. When the ANF is simulated in DCC and ICC methods, the APF can mitigate the harmonics. Comparing both methods, as shown by the THD values, the ICC method is more capable on mitigating harmonics compared to the DCC method. However, in consideration as extraction method for APF, the ANF is functioning perfectly as the extraction method.

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