# Combined Effect of a Catalytic Reduction Devicewith Waste Frying Oil-Based Biodiesel on NO<sub>x</sub> Emissions of Diesel Engines

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# Abstract

Internal combustion engines with application in automobiles and other rele- vant industries constitute significant environmental pollution via the release of toxic exhaust gasses like carbon monoxide (CO), hydrocarbons (HC), particulate matter (PM), and nitrogen oxide (NO<sub>x</sub>). Engine researchers and man- ufacturers are challenged to develop external and internal measures to ensure environmentally friendly solutions to accommodate and conform to the growing list of emission standards. Therefore, this work presents an experimental investigation of the NO<sub>x</sub> emission profile of a diesel engine that is fuelled and fitted with waste frying oil-based biodiesel and catalytic converter. Using a singlecylinder, four-stroke air-cooled CI engine at a constant speed of 1900 rpm and different loadings of 25%, 50%, 75%, and 100%; fitted with a catalyt- ic converter at the exhaust outlet of the engine and linked to a dynamometer and a gas analyser, an experiment was conducted at biodiesel/diesel volume blends of B0 (0/10), B5 (5/95), B20 (20/80), B30 (30/70), B70 (70/30), B100

(100/0); and 30% concentration (v/v), 0.5 litre/hr flow rate of aqueous urea from the catalytic converter. The results show an increasing NO<sub>x</sub> emission as the biodiesel component increased in the blend. The catalytic converter showed a downward NO<sub>x</sub> reduction with a significant 68% reduction in efficiency at high exhaust gas temperatures. It is concluded that the combined utilisation of waste frying oil-based biodiesel and the catalytic converter yields substan-tial NO<sub>x</sub> emission reduction.

# **Keywords**

Catalytic Converter, Waste Frying Oil, Biodiesel, NO<sub>x</sub> Emission, DieselEngines

### **1. Introduction**

The emissions from internal combustion engines (IC) include but are not limited to;  $NO_x$ , CO, hydrocarbons (HCs), and particulate matter. A singular IC engine such as an automotive engine will expel an insignificant amount of  $NO_x$  into the atmosphere. However, collectively in a group, internal combustion engines emit most of the total anthropogenic  $NO_x$ . For more than three decades, regulatory agencies have addressed  $NO_x$  emissions; however, there is an appetite for more stringent  $NO_x$  control measures beyond current requirements. The appetite for more stringent  $NO_x$  control is based on the role that  $NO_x$  emission plays in the development of ground-level ozone and photochemical smog (EPA, 2002 [1]); (Clean Air Technology Center, 1999 [2]). Biodiesel is a fuel type that continues to be evaluated as replacing diesel fuel in the automotive industry. Although it is sourced from many materials such as cooking oil and animal fat, it is cleaner, renewable. It can serve as a suitable replacement or an additive to diesel fuel. More so, it offers a high heat content, high density, and better lubricating prop- erties (Barabas and Todoru, 2012 [3]; Shahid and Jamal, 2011 [4]; Murugesan *et al.* 2009 [5]; Fasogbon and Asere, 2014 [6]). In addition, biodiesel is very differ- ent from conventional diesel due to its physicochemical properties. However, with biodiesel, there is reduced emission of carbon monoxide (CO), particulate matter (PM), and hydrocarbon (HC), it also causes higher NO<sub>x</sub> emissions pri- marily because of the presence of oxygen in the oil (Murugesan *et al.*, 2009 [5]; Fasogbon, 2015 [7]).

A literature review has shown that NO<sub>x</sub> emissions vary when diesel engines are fired with biodiesel produced from different organic sources. For example, Thangavelu and Thamilkolundhu, 2011 [8] evaluated the combustion and emis-sion characteristics of compression ignition (CI) engine fueled with Jatropha- diesel oil blends and observed the emissions include but are not limited to; NO<sub>x</sub>emission and combustion characteristics of the blends to be comparatively higher than that of the baseline diesel. In addition, Vallinayagam *et al.*, 2013 [9] also investigated a Kirloskar stationary CI engine fueled using pine oil blends whileloading the engine with an eddy current dynamometer at varying loads. The study observed a significant reduction in NO<sub>x</sub> emission by 15.2% compared to pure diesel and concluded that pine oil biofuel positively impacts the atmos- phere.

Although research is still ongoing on improving the quality and yield of bio- diesel from waste frying oil (WFO), the idea of converting WFO to biodiesel ori- ginates from the perspective of a waste management approach (Banerjee *et al.*,2014 [10]). The significant characteristics of WFOs concern high levels of free fatty acids, density, and viscosity. However, in producing biodiesel from WFOs, several factors such as; the type of oil source, duration of use, and the nature of the fried food products largely influence the quality of the biodiesel for use as fuel (Al-Kofahi, 2017 [11]; Shaban, 2018 [12]). Interestingly, with waste frying oil (WFO) biodiesel, studies have shown variations in NO<sub>x</sub> emission, for exam- ple, Al-Kofahi, 2017 [11]; Guo *et al.*, 2012 [13]; and Sanli, 2018 [14], reported an increase in NO<sub>x</sub> emission when using pure WFO biodiesel as against using pure diesel while Koçak *et al.*, 2007 [15], and Utlu *et al.*, 2008 [16], reported a de- crease in NO<sub>x</sub> emission and some others have reported no significant effect on the NO<sub>x</sub> emission (Dennis, 2001 [17]). The variations in the NO<sub>x</sub> emission due to engine combustion condi- tions and the differences in the chemical properties of the WFO as well as the in- fluence of the injection timing and the subsequent premixed and diffusion burn characteristics during combustion (Benjumea *et al.*, 2011 [14]; Guo *et al.*, 2012 [18]). However, with the SCR technology, NO<sub>x</sub> emission from diesel engines po- wered with WFO biodiesel has significantly reduced.

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The Selective Catalytic Reduction (SCR) method is an efficient approach to reducing  $NO_x$  emissions from biodieselfueled CI engines (Sala et al., 2018 [19]; Yang et al., 2015 [20]). Its principle is based on injecting a reducing agent (urea) into the exhaust gas flow stream of an internal combustion engine. The urea im- mediately converts to ammonia, and the ammonia reacts with the nitrogen oxide in the presence of a catalyst to produce nitrogen and water as the exhaust (EPA,2002 [1]; Sinzenich, 2015 [21]). With diesel fuel, the SCR system is considered a more effective means of reducing NO<sub>x</sub> emission (Sala *et al.*, 2018 [19]; Clean Air Technology Center, 1999 [2]). However, the SCR technology application is faced with some challenges. One of such challenges is the need to achieve a threshold temperature of about 200°C before injecting the urea solution into the hot ex- haust gas, which in most cases is above the exhaust gas temperature (Kröcher, 2018 [22]). To address this challenge, Sala et al., 2017 [23] in an experiment preheated and evaporated the urea solution before injecting it into the engine exhaust gas. In addition, while using biodiesel with SCR technology, because of the high concentration of impurities (potassium in the biodiesel), the catalyst [mostly V<sub>2</sub>O<sub>5</sub>-WO<sub>3</sub>/TiO<sub>2</sub> (VWT) vanadium/titanium-based] has been observed to be deactivated due to the neutralization of the catalyst's acid sites by the high ba- sicity content of the potassium, thus decreasing the adsorption of NH<sub>3</sub> (Kröcher, 2018 [22]; Schill and Fehrmann, 2018 [24]). Several studies have considered us-ing SCR technology alongside biodiesel blends to further investigate and reduce the  $NO_x$  emission from diesel engines. For example, Sundarraj *et al.*, 2014 [25] achieved a maximum of 73.94% reduction in NO<sub>x</sub> emission using a urea-SCR system (with a urea concentration of 32.5%, at a constant flow rate of 0.75 lit/hr.) fitted to a CI engine operating at different loading conditions and fuelled with diesel-jatropha blends (25% of Jatropha and 75% diesel blends).

More so, Praveen and Natarajan, 2014 [26] fueled a CI engine using a diesel- ethanol blend and observed a 70% reduction in NO<sub>x</sub> emission while using a cat- alytic converter (TiO<sub>2</sub>)-coated catalyst with 5% urea concentration, at a constant flow rate of 0.75 litre per hr. as against 66% reduction in NO<sub>x</sub> emission obtained when the engine was fueled with pure diesel, and 76.9% reduction was also rec- orded in another study that combines both an SCR device and an exhaust gas re- circulation (EGR) approach (Praveen and Natarajan, 2014 [26]; Praveena *et al.*, 2022 [27]). Consequently, it can be concluded that biodiesel blends nonetheless, when coupled with an SCR technology, and without any engine calibration or modifications would produce a significant reduction in NO<sub>x</sub> emission in the range of 58% to 75% (Shi *et al.*, 2008 [28]; Praveen and Natarajan, 2014 [26]; Sa-la *et al.*, 2018 [19]; Sundarraj *et al.*, 2014 [25]; Vallinayagam *et al.*, 2013 [9]; Yu-suf *et al.*, 2022 [29]). In sum, a relevant review pertaining to this research is provided in [30].

This study primarily observes the  $NO_x$  emission from a diesel engine fueled using biodiesel blends obtained from waste frying oil (WFO) and investigates the influence of a small-scale selective catalytic converter on the  $NO_x$  emission. The objective of the study is limited to examining the level of nitrogen oxide re-duction with the catalytic converter when firing with a WFO biodiesel blend. It, however, does not cover the analysis of the biodiesel effect on the catalyst, andneither does it evaluate the engine performance while operating with the WFO biodiesel.

### Materials and Methods

### **Biodiesel Production**

This study produced biodiesel from waste vegetable cooking oil via a transesteri- fication process as followed in previous studies by Dennis, 2001 [17]; Guo et al., 2012 [14]; Kocak et al., 2007 [16]; and Tziourtzioumis et al., 2017 [31]. The waste cooking oil sample was collected from roadside bean cake and fried yam sellers on the streets of Agbowo, Ibadan, Nigeria. Using a simple transesterification batch process, 10.5 millilitres of the waste cooking oil sample was measured, filtered to remove residues and unwanted particles, poured into a 250 milliliter conical flask, and heated to a preselected temperature of 50°C. A solution of potassium me- thoxide was equally produced using 0.25 g of potassium hydroxide pellet and 63millilitres of methanol (catalyst concentration of 0.5% and an oil/Methanol mole ratio of 1:6). The potassium hydroxide pellet was stirred vigorously until it dis-solved completely in the methanol mixture. The potassium methoxide solution was then mixed with the warm waste cooking oil, stirred vigorously with a me-chanical stirrer while heating until 60°C for about 50 minutes. The solution waskept to cool and settle for a day and later transferred to a gravity separating fun-nel until two distinct layers were visible. The glycerol and residual catalyst were removed, while the biodiesel was extracted, washed with warm deionized water, and heated to 30°C to remove water. The WFO based produced biodiesel was characterised and the results presented in Table 1 and the expected standard for biodiesel properties. Diesel engine test rig for biodiesel-diesel blends with speci- fications is detailed in Table 2. The biodiesel blends were; pure diesel [B0]-0% biodiesel and 100% diesel [B100]; [B5]-5% biodiesel and 95% diesel; [B20]-20% biodiesel and 80% diesel; [B30]-30% biodiesel and 70% diesel; [B70]-70% bio- diesel and 30% diesel [B100]-00% biodiesel and 0% diesel.

Table 2. Test engine specifications. Make: Kama KM170F Air Cooled Diesel Engine Parameter Notes/Values Combustion system Direct injection No of cylinder Single cylinder Max output 2.8 kw - 3.1 kw Con output 2.5 kw - 2.8 kw Engine speed 3000 rpm - 3600 rpm Bore × stroke  $70 \text{ mm} \times 55 \text{ mm}$ Fuel used Light diesel oil Displacement 0.211 Fuel tank capacity 2.5 L Starting system Recoil or electric starter

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### **The Selective Catalytic Converter and Reagent**

The study developed a catalytic converter similar to those previously developed by Tan *et al.*, 2020 [32]; and Bhaskarrao and Shinde, 2015 [33]. The catalytic converter had a honeycomb structure with a cylindrical shell with length and diameter, approximately 92 mm and 69 mm, respectively. It had a converter vo-lume of 0.3393 litres (339.23 cc), designed for an exhaust gas volume flow rate of  $0.006349 \text{ m}^3$ /sec. It had a platinum catalyst and a wash-coat coated with an alloy of Al<sub>2</sub>O<sub>3</sub>. The reagent system, however, consists mainly of the following compo- nents: a storage tank, a dc pump, piping, a time relay-delay module to regulate the injection timing of the warm aqueous urea solution, an atomizer nozzle, anda 12-volt battery to power the dc pump and the relay-delay module. The study utilized a warm anhydrous aqueous urea of 30% concentration (volume/volume %)at 40°C stored in a plastic container tightly covered to prevent contamination and for ease of handling and simplicity of design. Although the scope of this study does not cover the analysis on the effect of reagent concentration on the converter, however, the reagent set-up follows a similar approach and set-up puttogether in the study by Sundarraj *et al.*, 2014 [25]; Vallinayagam *et al.*, 2013 [9];and Kumar *et al.*, 2021 [34].

### **Experimentation**

Praveena *et al.*, 2022 [27]; Kumar *et al.*, 2021 [34]; and Vallinayagam *et al.*, 2013[9] developed a similar experimental set-up to those used in this research, as shown in Figure 1. The experiment was conducted using a four-stroke, air-cooled C.I engine with the specification given in Table 2, fueled with biodiesel blends



Figure 1. Experimental configuration.

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[B0], [B5], [B20], [B30], [B70], and [B100], and operating at a constant engine speed of 1900 rpm. The engine was connected to a Megatech DG2 dynamometer for loading varying from 25%, 50%, 75%, and 100% full load, a PCA 3 BacharachGas analyzer also connected to a computer for data collection, and the catalyticconverter connected at the exhaust gas outlet tail end of the diesel engine, as shown in **Figure 1**. The warm aqueous urea stored in a container was metered and injected (using a time relay-delay module and a dc pump connected to a 12-volt battery) into the exhaust gas flow stream through a fine atomizer nozzle fixed upstream of the exhaust gas flow. The experiment maintained the proce- dure over time while varying the engine load; the NO<sub>x</sub> emission data were col-lected, and the graphs presented the results.

# **Results and Discussions**

The exhaust gas temperature and  $NO_x$  emission against different load ranges are plotted for the base fuel diesel [B0], pure biodiesel [B100], and the various bio-diesel blends [B5], [B20], [B30], and [B70].

# Exhaust Gas Temperature at Different Load Ranges

The necessary information on performance characteristics of relevant systems could be found in the work of Utlu *et al.*, 2008 [15]. Although performance cha- racteristics are not the focus of this work, the extraction of exhaust gas temperature provides an understanding of  $NO_x$  emission. Figure 2 depicts the exhaust gas temperature relative to the load percentage revealing an increasing trend.

### NO<sub>x</sub> Profile without the Use of the Catalytic Converter

**Figure 3** shows a plot of  $NO_x$  emission against biodiesel-fossil diesel blends with- out catalytic converter as an add-on technology at different loadings. It was ob-served that an increasing percentage of biodiesel in biodiesel-fossil diesel blends leads to an increase in  $NO_x$  emission. And this observation is in tandem with Shahid *et al.*, 2011 [4] and Fasogbon, 2015 [7]. The study observed that the oxy- gen richness of biodiesel could have been responsible for the increasing content NO<sub>x</sub>; as the higher the exhaust gas temperature, the higher the  $NO_x$  emission. Thus, the oxygen content/richness of Waste Frying Oil-based biodiesel must have supported combustion; thereby leading to high  $NO_x$  emission emanating from high exhaust gas temperature.

### NO<sub>x</sub> Profile with the Use of the Catalytic Converter

Even though the increasing percentage of biodiesel in biodiesel-fossil diesel blends leads to an increase in  $NO_x$  emission, as in the case of Figure 3, the in- jection of a catalytic converter as an add-on technology/device significantly reduces  $NO_x$  emission, as shown in Figure 4. At higher engine loads which is equivalent to higher exhaust gas temperature and  $NO_x$  emission, there were higher reductions of  $NO_x$ ; this is because, at the higher temperature, Ammonia





Figure 3. Plot of  $NO_x$  emissions for biodiesel blends without the use of the catalytic converter device.



Figure 4. Plot of  $NO_x$  emissions for biodiesel blends with the use of the catalytic converter device.

(Urea reagents) do show better reaction with NO<sub>x</sub>. This observation is in linewith the work of Sala et al., 2017 [23].

### Conclusion

This study ascertained the  $NO_x$  emission profile of a diesel engine powered with a Waste frying oil-based biodiesel at different blends and further evaluated a cat- alytic converter's  $NO_x$  emission reduction efficiency. With the conclusion that a combined effect of waste frying oil-based biodiesel and catalytic converter as add-on technology will yield a significant  $NO_x$  emission reduction.

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